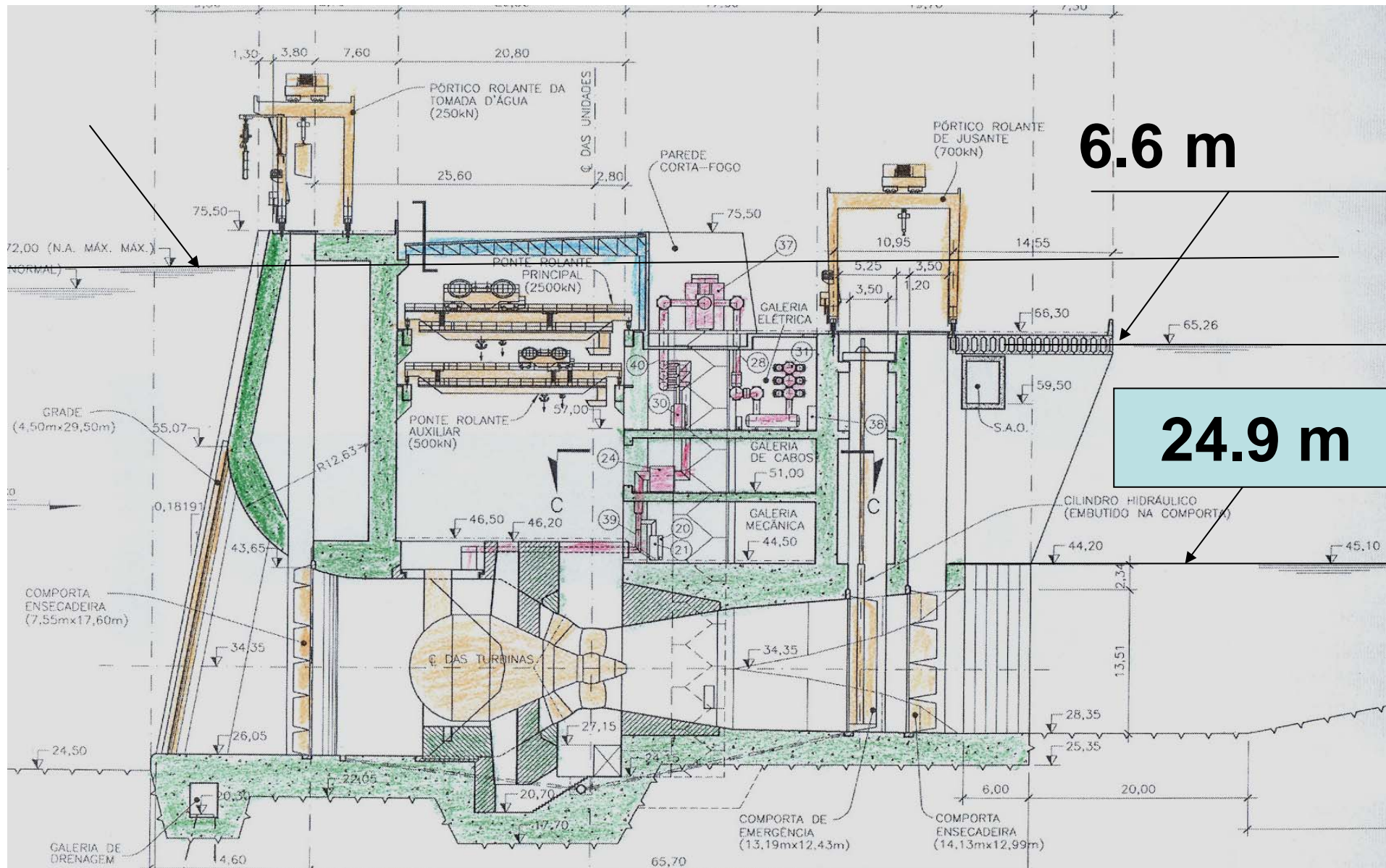


STUDY OF TURBINE DESIGN, CONTROL SYSTEMS AND POWER PRODUCTION FOR SANTO ANTÔNIO PROJECT

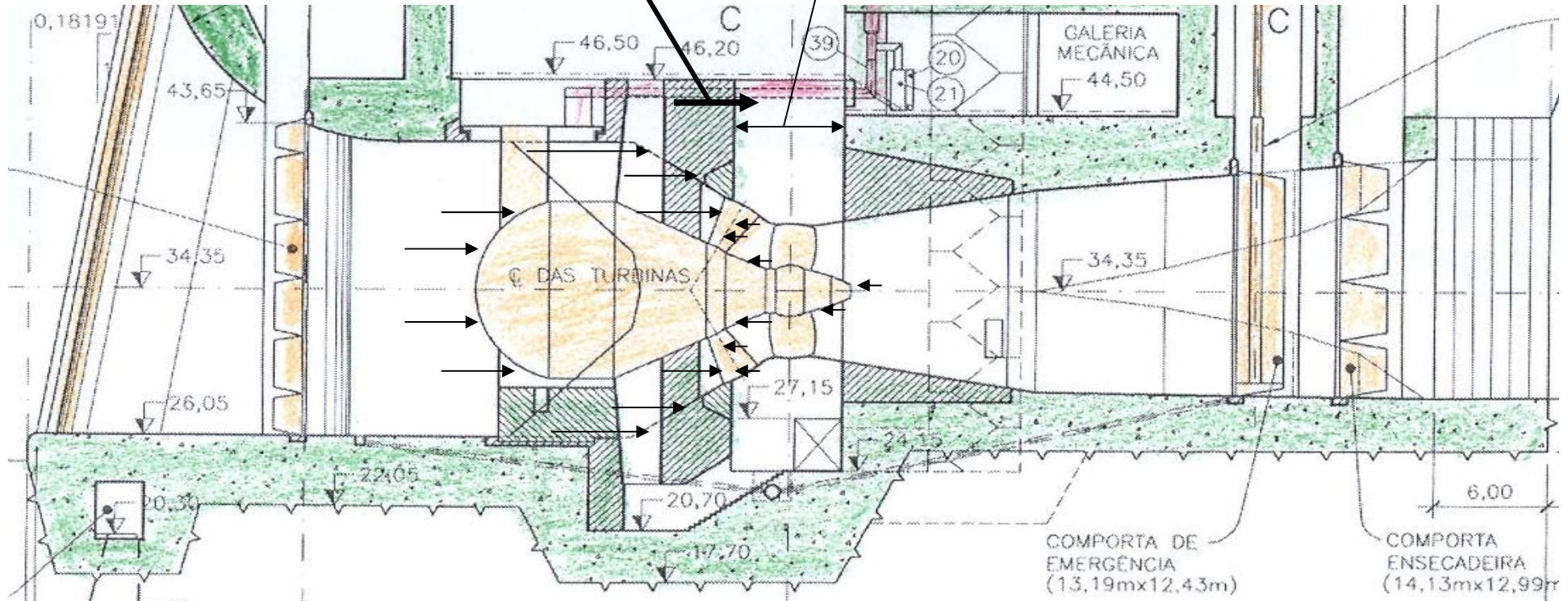
- 1. CHOICE BETWEEN KAPLAN AND BULB TURBINES.**
- 2. OPERATION LIMITATIONS BECAUSE OF LARGE VARIATIONS IN FLOW AND WATER LEVEL.**
- 3. HYDRAULIC FORCES FROM TURBINES ON POWER HOUSE AND THRUST BEARINGS.**
- 4. POSSIBLE SAND EROSION PROBLEMS.**
- 5. POSSIBLE CONTROL PROBLEMS OF TURBINES.**
- 6. MATERIAL QUALITY AND STANDARDS, BRAZILIAN PRODUCTION**



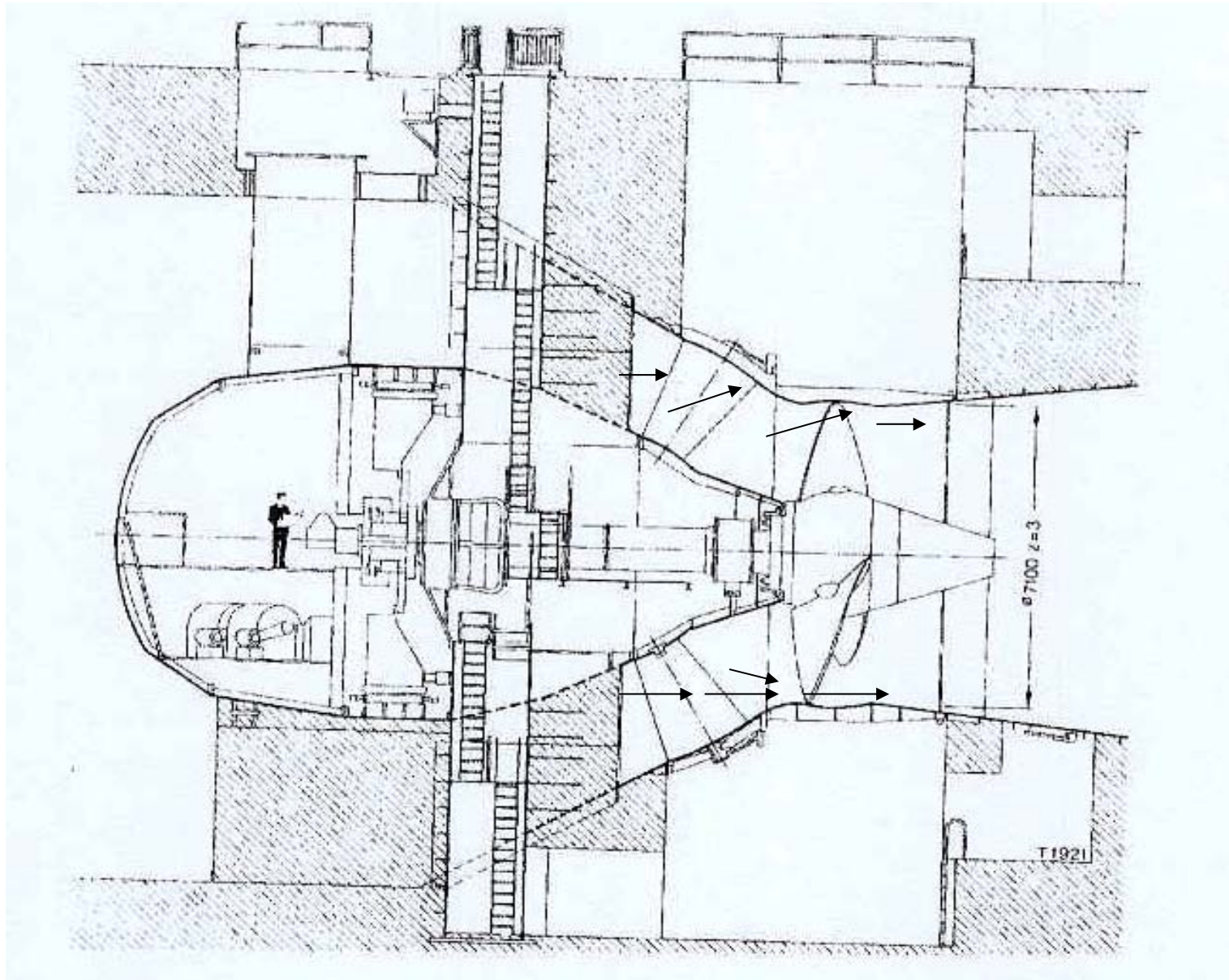
Hydraulic forces on concrete.

OPENING NOT TO BE REDUCED (MAX. 3-5 mm)

8158 TONN



SAND EROSION

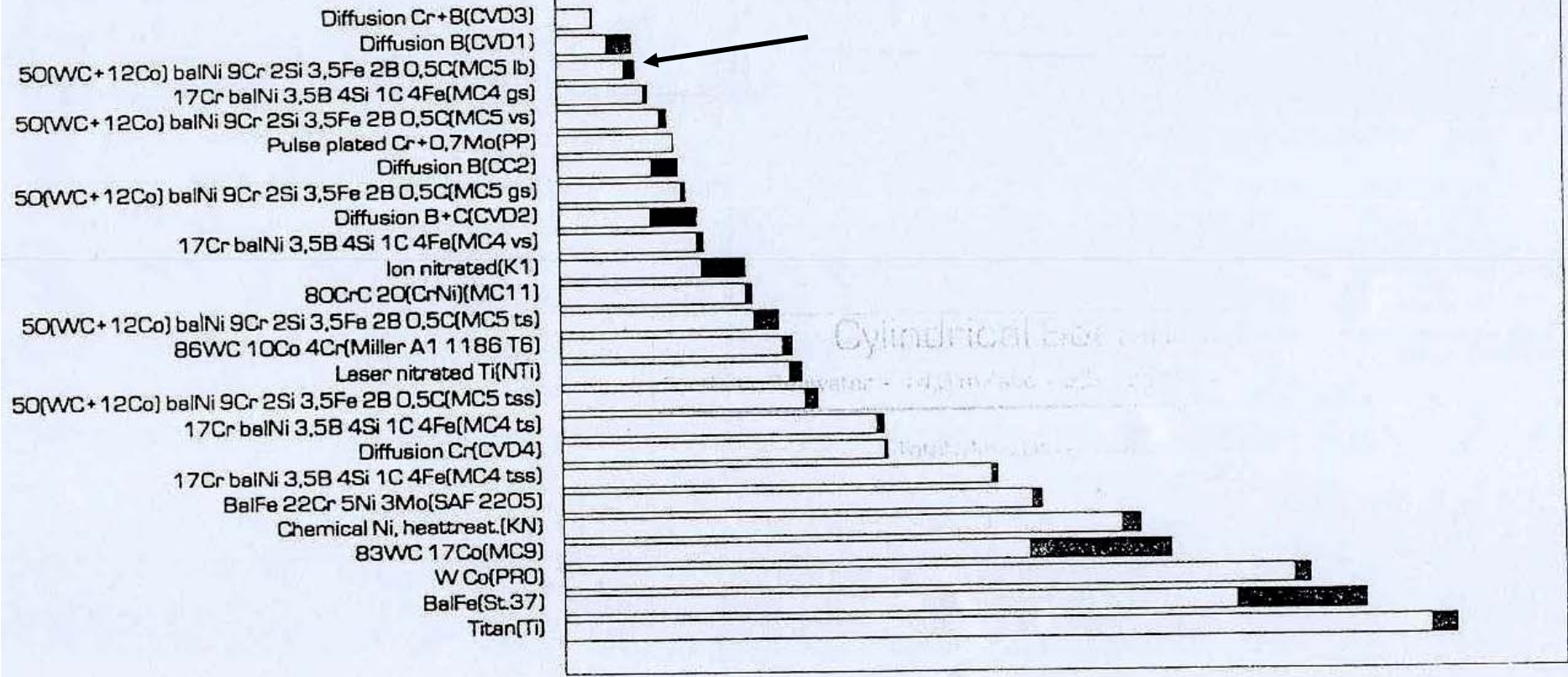


NORWEGIAN RESEARCH ON HARD SURFACE COATING

Cylindrical Specimens
 Synthetic Seawater - 14,3 m/sec - 2,5% sand - Airsaturated - 20°C

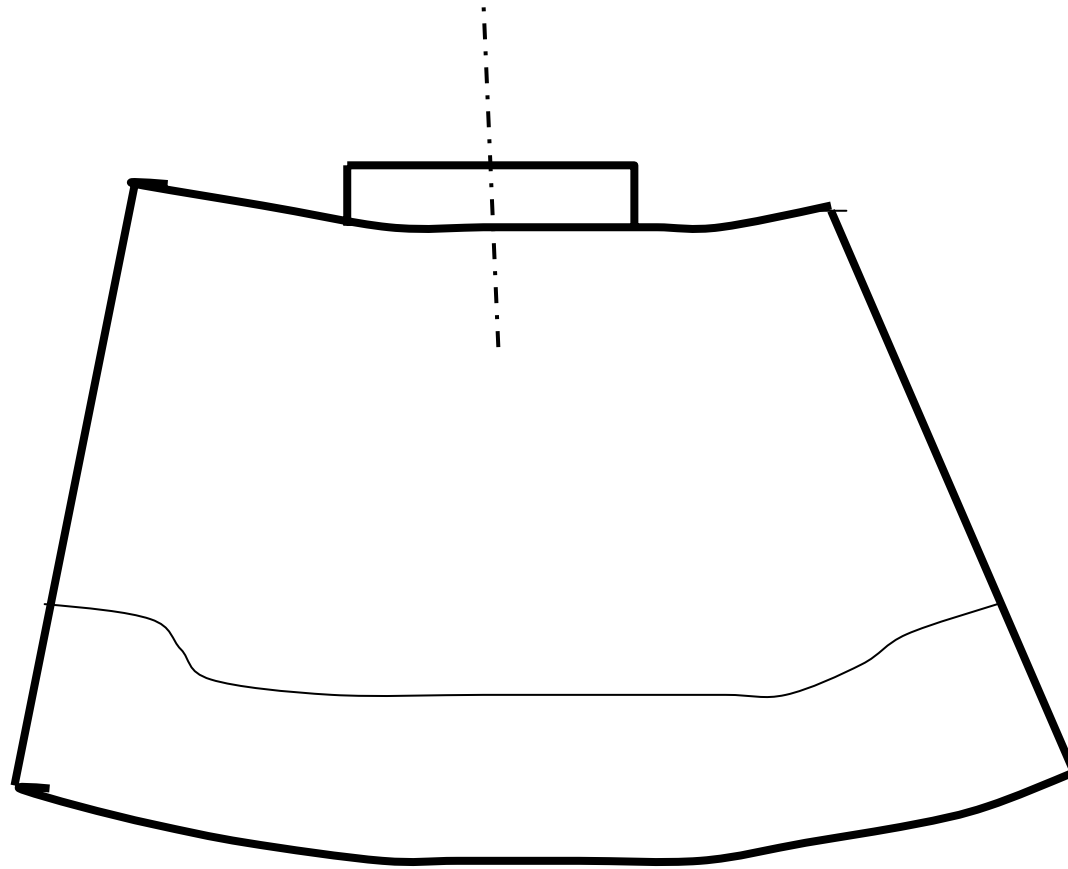
Total Mass Loss (mm/year)

0 2 4 6 8 10 12 14 16 18

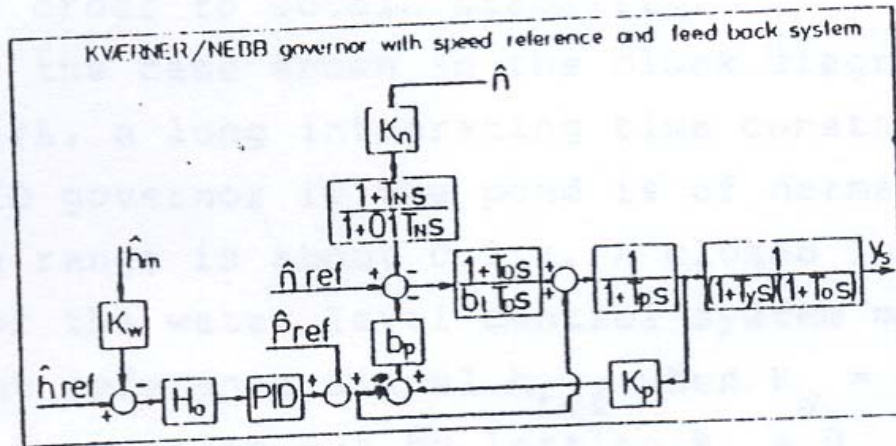


■ Corrosion

COATING OF RUNNER BLADES



FREQUENCY STABILITY ON POWER LINES ? LEIGHT WEIGHT GENERATORS, UNSTABLE TURBINES.



From the block diagram it is substituted for different transferfunctions as shown

G = the turbine governor as shown with dotted lines
Further:

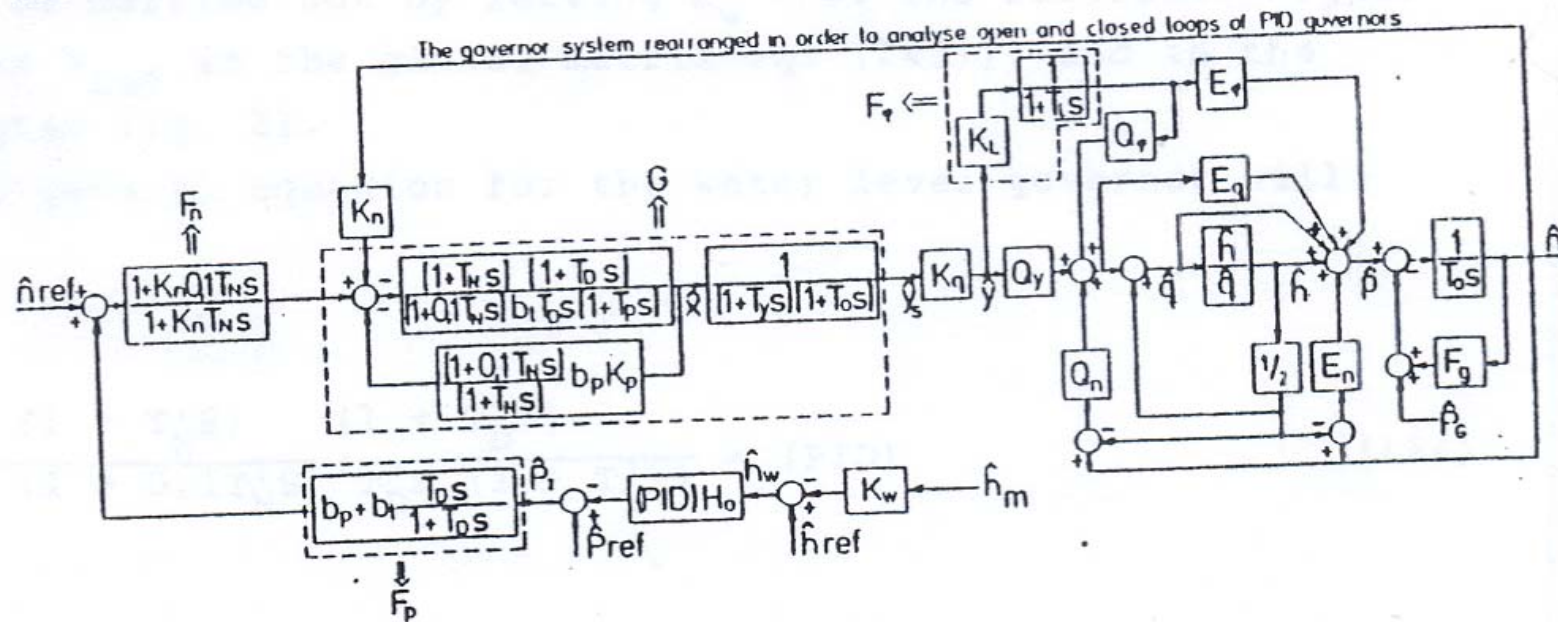
$$F_n = \frac{1 + K_n 0.1 T_n s}{1 + K_n T_n s}, \quad F_p = (b_p + b_i \frac{T_D s}{1 + T_D s})$$

$$F_\phi = K_L \frac{1}{1 + T_L s}$$

The PID governor for external governors as a water level controller may principally be described as

$$PID = \frac{1}{b_i} \frac{(1 + T_{ii} s)}{(1 + 0.1 T_n s)} \frac{(1 + T_D s)}{T_D s (1 + T_D s)}$$

(Note b_i may be negative for w.l. control downstream of turbine.)



THE MOST IMPORTANT STANDARDS YIELDS:

- **FOR ELECTROMECHANICAL EQUIPMENT:
IEC NORMS , BULB TURBINES
= TUBULAR TURBINES IEC 61366-5**
- **FOR STEEL CASTINGS: CCH 70-3**
- **BRAZILIAN INDUSTRY MEETS THESE
STANDARDS IN MOST CASES.**